

5 Magnetic Circuits

Student Group

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5. Magnetic Circuits

For this and the following chapter the online Book 'DC Electrical Circuit Analysis - A Practical Approach' is strongly recommended as reference. In detail this is chapter [10.3 Magnetic Circuits](#)

- [Gyrator-capacitor model](#)

In the previous chapters we got accustomed to the magnetic field. During this path some similarities from the magnetic field to the electric circuit appeared (see [figure 1](#)).

Fig. 1: Similarities magnetic Circuit vs electric Circuit

In this chapter we will investigate, how far we come with such an analogy and where it can be practically applied.

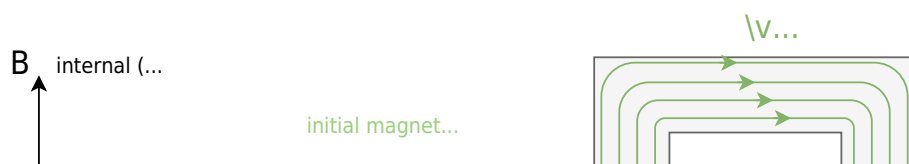
5.1 Linear magnetic Circuits

For the upcoming calculations the following assumptions are made

1. The relationship between B and H is linear: $B = \mu \cdot H$
This is a good estimation when the magnetic field strength lies well below saturation
2. There is no stray field leaking out of the magnetic-field conducting material.
3. The fields inside of airgaps are homogeneous. This is true for small airgaps.

One can calculate a lot of simple magnetic circuits, when these assumptions and focusing on the average field line are applied.

Fig. 2: Simplifications and Linearization



Two simple magnetic circuits are shown in [figure 3](#): They consist of

- a current-carrying coil
- a ferrite core
- an airgap (in picture (2)).

Fig. 3: A simple magnetic Circuit



These three parts will be investigated shortly:

Current-carrying Coil

For the magnetic circuit, the coil is parameterized only by:

- its number of windings N and
- the passing current i .

These parameters lead to the magnetic voltage $\mathcal{U} = N \cdot i$.

Ferrite Core

- The core is assumed to be made of ferromagnetic material.
- Therefore, the relative permeability in the core is much larger than in air ($\mu_{r,core} \gg 1$).
- The ferrite core is also filling the inside of the current-carrying coil.
- The ferrite core conducts the magnetic flux around the magnetic circuit (and by this: also to the airgap)

Airgap

- The airgap interrupts the ferrite core.
- The width of the airgap is small compared to the dimensions of the cross section of the ferrite core.
- The field in the airgap can be used to generate (mechanical) effects within the airgap.
An example for this can be the force onto a permanent magnet (see [figure 3 \(3\)](#)).

With the above-mentioned assumptions the magnetic flux Φ must remain constant along the ferrite core, so $\Phi_{core} = \text{const.}$

Since the magnetic field lines neither show sources nor sinks, also the flux passing over to the airgap must be $\Phi_{airgap} = \Phi_{core} = \text{const.}$ This can also be seen in [figure 4 \(1\)](#).

A different view onto this is the closed surface $\vec{A}$ (figure 4 (2)): Based on the examination in [Recap of magnetic Field](#) we know that the flux into the volume must be equal the flux out of the volume, or $\Phi_m = \oint_A \vec{B} \cdot d\vec{A} = 0$.

The relationship $B = \mu \cdot H$, and $\mu_{\text{core}} \gg \mu_{\text{airgap}}$ lead to the fact that the H -Field must be much stronger within the airgap (figure 4 (3)).

Fig. 4: B- and H-field along the ferrite core



Magnetic Circuit in a Formula

Therefore, the following formula is given
$$\Phi_m = \oint_A \vec{B} \cdot d\vec{A} = \text{const.} \cdot \oint \vec{B} \cdot d\vec{A} = \text{const.} \cdot \oint \vec{B}_{\text{core}} \cdot d\vec{A}_{\text{core}} = \vec{B}_{\text{airgap}} \cdot d\vec{A}_{\text{airgap}} = \text{const.}$$

The assumptions, that there is that the field inside of airgap is homogenous and there is no strayfield lead to the fact, that $A_{\text{core}} = A_{\text{airgap}}$.

Therefore:
$$\vec{B}_{\text{core}} = \vec{B}_{\text{airgap}} = B \cdot \mu_0 \mu_{r,\text{core}} H_{\text{core}} = \mu_0 \mu_{r,\text{airgap}} H_{\text{airgap}} = \frac{\Phi}{A} \tag{5.2.1}$$

Beside this, the magnetic field strength H along one field line is directly given by:
$$\oint \vec{H} \cdot d\vec{s} = \oint_{\text{core}} \vec{H} \cdot d\vec{s} + \oint_{\text{airgap}} \vec{H} \cdot d\vec{s}$$

With the assumption of a linear and homogeneous B -Field and the width δ of the airgap, this leads to:
$$\oint \vec{H} \cdot d\vec{s} = H_{\text{core}} l_{\text{core}} + H_{\text{airgap}} \delta \tag{5.2.2}$$

With the previous formula 5.2.1, this gets to:
$$\oint \vec{H} \cdot d\vec{s} = \frac{B}{\mu_0 \mu_{r,\text{core}}} l_{\text{core}} + \frac{B}{\mu_0 \mu_{r,\text{airgap}}} \delta = \frac{\Phi \cdot l_{\text{core}}}{A \cdot \mu_0 \mu_{r,\text{core}}} + \frac{\Phi \cdot \delta}{A \cdot \mu_0 \mu_{r,\text{airgap}}} = \frac{1}{\mu_0 \mu_{r,\text{core}}} \frac{l_{\text{core}}}{A} \Phi + \frac{1}{\mu_0 \mu_{r,\text{airgap}}} \frac{\delta}{A} \Phi \tag{5.2.3}$$

Comparing the formula 5.2.3 with the ohmic resistance and resistivity of two resistors in series, shows something interesting:
$$U = R_1 \cdot i + R_2 \cdot i = \rho \frac{l_1}{A_1} \cdot i + \rho \frac{l_2}{A_2} \cdot i$$

This leads to:

- The magnetic voltage $\oint \vec{H} \cdot d\vec{s}$ acts like the electric voltage U ,

the magnetic flux Φ like the current i .

- The linear relationship $\theta = f(\Phi)$ is also called [Hopkinson's Law](#).

Notice:

- Also for the magnetic circuit one can set up a lumped circuit model (see [figure 5](#)).
- Similar to Ohms law, there is a **magnetic resistance** or **reluctance**:

$$R_m = \frac{1}{\mu_0 \mu_r} \frac{l}{A}$$
- The unit of R_m is $[R_m] = [\theta]/[\Phi] = 1 \text{ A} / \text{Vs} = 1/\text{H}$
- The length l is given by the average field line length in the core.
- The Kirchhoff's laws (mesh rule and nodal rule) can also be applied:
 - The sum of the magnetic fluxes Φ_i in into a node is: $\sum_i \Phi_i = 0$
 - The sum of the magnetic voltages θ_i along the average field line is:
 $\sum_i \theta_i = 0$
- The application of the lumped circuit model is based on multiple assumptions.
 In contrast to the simplification for the electric current and voltage the simplification for the flux and magnetic voltage is not as exact.

Fig. 5: lumped Circuit Model for magnetic Circuits

Application and Limitations of the Circuit Interpretation

Notice:

“Recipe” for solving magnetic circuits:

1. Watch out for individual magnetic resistances in the circuits:
 1. Separate the magnetic circuit into parts, where the permeability and area of the cross section is constant.
For these parts B and H is constant. These parts will have individual magnetic resistances.
 2. Each airgap also get an individual magnetic resistance.
 3. Calculate the magnetic resistance by the average length of field line through the individual parts.
2. Calculate the magnetic circuit as circuit.
 1. Magnetic voltages depicts voltage sources ; magnetic flux depicts currents.
 2. Use the known way to solve the circuit.

Be aware that the orientation of the current I and the field strength $\vec{H}$ are also connected by the right hand rule.

The results are only allowed as first approximation. The following table shows the contrast between the electric and magnetic field:

Property	Electric Field	Magnetic Field
Materials	There are "pure" isolator, which are completely non conductive.	All materials have a permeability >0
Sources	The source is concentrated (= there are field sources / electric charges)	The magnetic source (= coil) is distributed
Simplifications	The simplifications often work for good results (small wire diameter, relatively constant resistivity)	The simplification are often too simple (wide spread beyond the average field length, non-linearity of the permeability)

Task 5.1.1 Coil on a plastic Core

A coil is set-up onto a toroidal plastic ring ($\mu_r=1$) with an average circumference of $l_R = 300\text{mm}$. The $N=400$ windings are evenly distributed along the circumference. The diameter on the cross section of the plastic ring is $d = 10\text{mm}$. In the windings a current of $I=500\text{mA}$ is flowing.

Calculate

1. the magnetic field strength H in the middle of the ring cross section.
2. the magnetic flux density B in the middle of the ring cross section.
3. the magnetic resistance R_m of the plastic ring.
4. the magnetic flux Φ .

Task 5.1.2 Coil on a ferrite Core with airgap

The choke coil shown in [figure 10](#) shall be given, with a constant cross section in all legs l_0 , l_1 , l_2 . The number of windings shall be N and the current through a single winding I .

Fig. 10: Example for a Choke Coil



1. Draw the lumped circuit of the magnetic system
2. Calculate all magnetic resistances $R_{m,i}$
3. Calculate the partial fluxes in all the legs of the circuit

5.2 Non-linear magnetic Circuits

not included in the present script

5.3 Mutual Induction and Coupling

Situation: Two coils \$1\$ and \$2\$ near by each other.

Questions:

- Which effect do the coils have onto each other?
- Can we describe the effects with mainly electric properties (i.e. no geometric properties)

Fig. 9: Mutual Induction of two Coils

Effect of Coils onto each other

1. Windings N_1 of coil \$1\$ gets feed with current i_1 .
 2. Coil \$1\$ generates change in flux Φ_{11}
 3. Coil \$2\$ gets passed by part of the flux (Φ_{21})
 4. Stray flux Φ_{S1} takes not part in coupling
- $\rightarrow$ Coils are magnetically coupled:
Flux Φ_{11} of coil \$1\$ gets divided into flux Φ_{21} in coil \$2\$ and stray flux Φ_{S1} not passing coil \$2\$:

$$\Phi_{11} = \Phi_{21} + \Phi_{S1}$$

- Induced voltage in coil \$2\$:

$$u_{\text{ind},2} = - \frac{d}{dt} \Psi_{21} \\ \quad \quad = -N_2 \cdot \frac{d}{dt} \Phi_{21}$$

- Similar effect on coil \$1\$ due to a current i_2 through coil \$2\$:

$$\Phi_{22} = \Phi_{12} + \Phi_{S2}$$

$$u_{\text{ind},1} = -N_1 \frac{d}{dt} \Phi_{12}$$

Linked Fluxes

For the single coil we got the relationship between the linked flux Ψ and the current i as: $\Psi = L \cdot i$.

Now the coils also are interacting with each other. This must also be reflected in the relationship $\Psi_1 = f(i_1, i_2)$, $\Psi_2 = f(i_1, i_2)$:

$$\begin{aligned} \Psi_1 &= \Psi_{11} + \Psi_{12} \\ \Psi_2 &= \Psi_{22} + \Psi_{21} \end{aligned}$$

$$\begin{aligned} \Psi_1 &= L_{11} i_1 + M_{12} i_2 \\ \Psi_2 &= L_{22} i_2 + M_{21} i_1 \end{aligned}$$

With

- L_{11} and L_{22} as the self induction
- M_{12} and M_{21} as the **mutual induction**

The formula can also be described as:

$$\begin{pmatrix} \Psi_1 \\ \Psi_2 \end{pmatrix} = \begin{pmatrix} L_{11} & M_{12} \\ M_{21} & L_{22} \end{pmatrix} \begin{pmatrix} i_1 \\ i_2 \end{pmatrix}$$

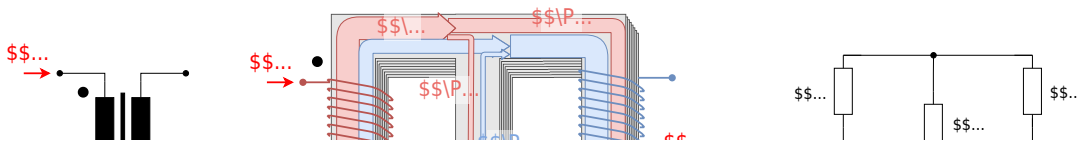
The main question is now: How do we get L_{11} , M_{12} , L_{22} , M_{21} ?

Magnetic Circuit with 2 Sources

In order to get the self induction and mutual induction of two interacting coils, we are going to investigate two coils on an iron core with a middle leg (see [figure 10](#)).

Then the stray flux of the previous situation is only located in the middle leg. This also means, that there is no stray flux outside of the iron core.

Fig. 10: Example for Iron Core with two Coils



The [figure 10](#) shows the fluxes on each parts. The filled black circles nearby the windings mark the direction of winding:

When there is one current for each winding ingoing into the marked pin, the fluxes will get added up positively.

In order to get L_{11} and L_{22} , we look back to the inductivity L of a long coil with the length l .

This was given in the chapter [Self-Induction](#) as

$$L = \frac{\Psi}{i} \quad L = \mu_0 \mu_r \cdot N^2 \cdot \frac{A}{l}$$

In this case, Ψ was the flux through the coil generated from the coil itself - here L_{11} and L_{22} .

Comparing this formula with the magnetic resistance $R_m = \frac{l}{\mu_0 \mu_r A}$ of the coil, one can conclude:

$$\boxed{L = \frac{N^2}{R_{m,coil}}}$$

Based on this formula, the self inductions L_{11} and L_{22} can be written with the magnetic resistances of the coils as:

$$L_{11} = \frac{N_1^2}{R_{m,11}} \quad L_{22} = \frac{N_2^2}{R_{m,22}}$$

In order to get the effect of the mutual induction, a coupling coefficient k is introduced. k_{21} describes how much of the flux from coil 1 is acting on coil 2 (similar for k_{12}):

$$k_{21} = \frac{\Phi_{21}}{\Phi_{11}}$$

When $k_{21} = 100\%$, there is no flux in the middle leg but only in the second coil.

For $k_{21}=0$ all the flux is in the middle leg circumventing the second coil, i.e. there is no coupling.

The resulting total coupling k is given as

$$k = \sqrt{k_{12} \cdot k_{21}}$$

The mutual induction M_{21} can be calculated as the fraction of the linked flux Ψ_{11} in coil 2 based on the current i_1 from the coil 1 :

$$\begin{aligned} M_{21} &= \frac{\Psi_{21}}{i_1} = \frac{N_2 \cdot \Phi_{21}}{i_1} = \frac{N_2 \cdot k_{21} \cdot \Phi_{11}}{i_1} = \frac{N_2}{N_1} k_{21} \cdot \frac{\Psi_{11}}{i_1} \\ &= \frac{N_2}{N_1} k_{21} \cdot L_{11} = \frac{N_2}{N_1} k_{21} \cdot \frac{N_1^2}{R_{m,11}} = k_{21} \cdot \frac{N_1 \cdot N_2}{R_{m,11}} \end{aligned}$$

The formula can also be described as:
$$\left(\begin{array}{c} \Psi_1 \\ \Psi_2 \end{array} \right) = \left(\begin{array}{c} \frac{N_1^2}{R_{m,11}} \\ \frac{N_1 \cdot N_2}{R_{m,12}} \\ \frac{N_2^2}{R_{m,22}} \end{array} \right) \cdot \left(\begin{array}{c} i_1 \\ i_2 \end{array} \right)$$

5.4 Magnetic Energy

Tasks

Task 5.1.4 Application: Shaded Pole Motor

The [figure 25](#) and [figure 25](#) show a shaded pole motor of a commercial oven.

- Find out how this motor works - explicitly: why is there a preferred direction of the motor?
- In which direction does the shown motor run?

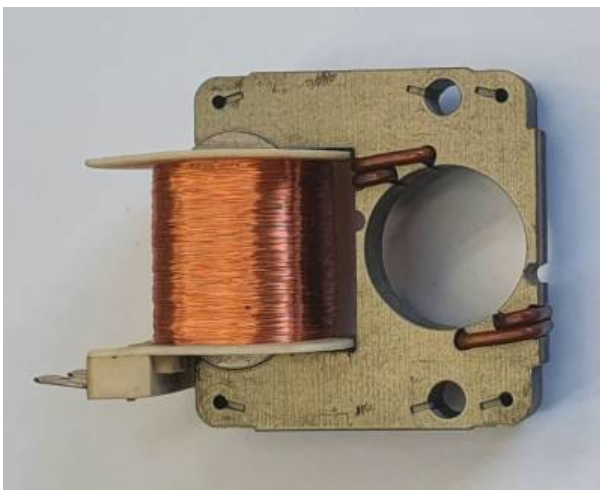


Fig. 25: Core of a shaded Pole Motor

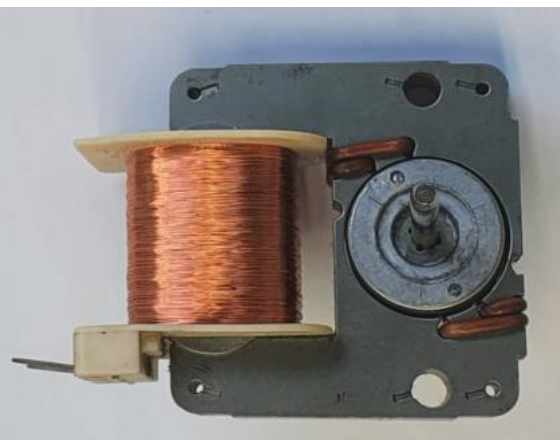
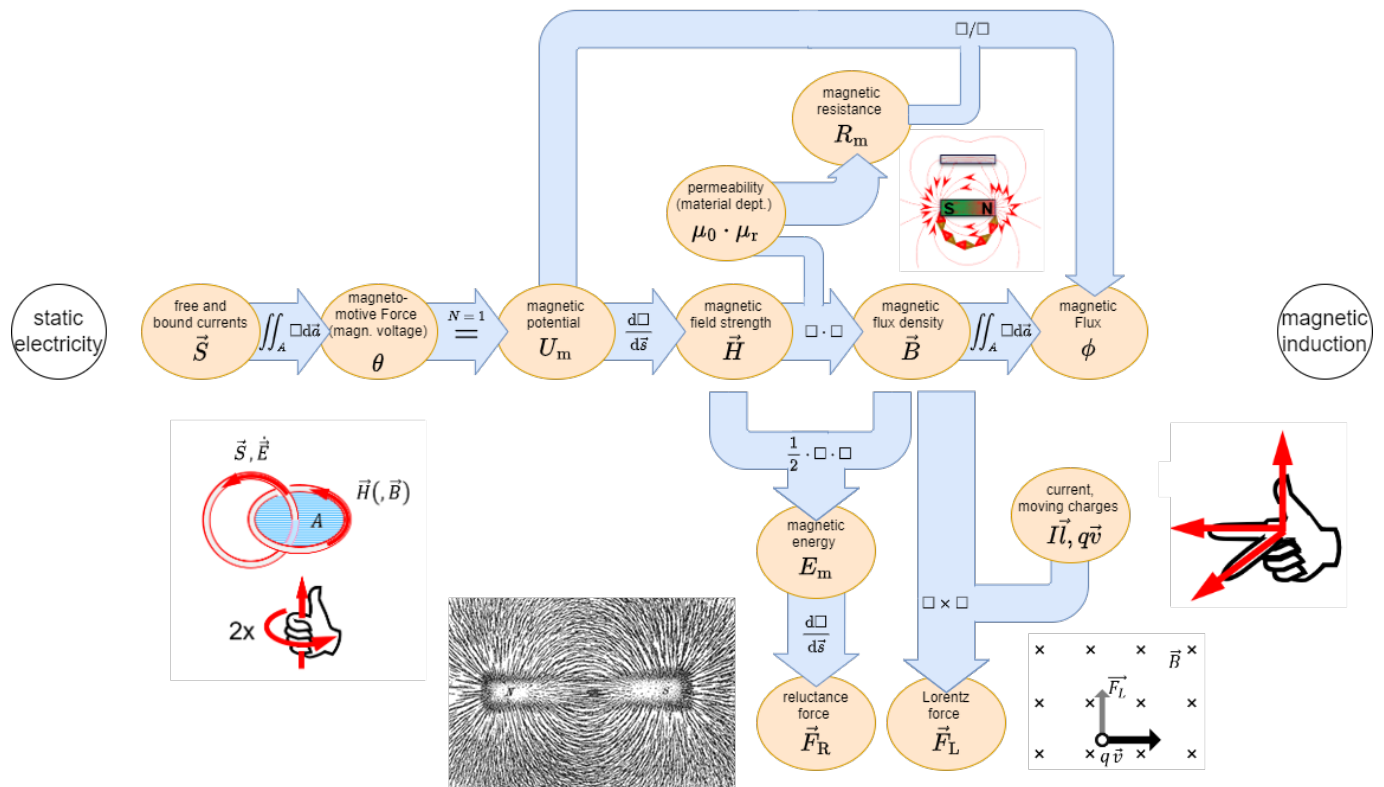


Fig. 26: Setup of the full shaded Pole Motor

Fig. 29: Overview of the magnetic Formalism



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